ERRATA

THERMAL RADIATION HEAT TRANSFER

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Page | Correction
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11 | Eq. (1.6): the RHS should be $2\pi$, not $4\pi$.
27 | Fig. 1.16: In the caption, replace “crosshatched” with “light gray”.
Second line in first paragraph, replace “crosshatched” with “light gray”.
28 | Fig. 1.17: On the x-axis, replace $10^0$ with $10^3$, and $10^1$ with $10^4$.
55 | In Figure 2.2e, on the incoming ray, replace $I_i(\theta_i, \phi_i, T_i)$ with $I_i(\theta_r, \phi_r, T_r)$.
In Figure 2.2e, on the reflected ray, replace $I_r(\theta, \phi, \theta_i, \phi_i, T_i)$ with $I_r(\theta, \phi, \theta_r, \phi_r, T_r)$.
In Figure 2.2e, for the reflected ray, the angles with respect to the axes should be $\theta_r$ and $\phi_r$, not $\theta$ and $\phi$.
Revise the caption to Figure 2.2 to read:
“Pictorial descriptions ……….., the subscript $\lambda$ is added to the property definitions: (a) ………; (e) bi-directional reflectivity $\rho(\theta_r, \phi_r, \theta_i, \phi_i, T_i)$; (f)………”
56 | In Figure 2.2i, for the incoming ray, replace the azimuthal angle $\theta_i$ with $\theta_r$.
In Figure 2.2i, for the transmitted ray, replace $I_t(\theta, \phi, \theta_i, \phi_i, T_i)$ with $I_t(\theta, \phi, \theta_r, \phi_r, T_r)$.
In the caption Figure 2.2 (Continued), second line, revise to read “….. the subscript $\lambda$ is added to the property……..”
63 | In the line after Eq. (2.11), replace $dA \cos \theta / R^2$ with $dA \cos \theta_r / R^2$.
At end of line after Eq. (2.11), add “….. as in Figure 2.7a.”
163 | In Eq. (4.15) the RHS should read $dA_i F_{dl-2}$.
187 | Fig. 4.24a: The element $dA_2$ is meant to be a strip element that goes completely around the interior of the square channel.
222 | In text line above Eq. (5.9.1), $\varepsilon_2$ should be plain text, not bold.
242 | The upper limit in Eq. (5.19.1) should be $\eta = l$, not $\eta = 1$.
273 | Section 6.2, first paragraph, at end of line modify to read "…..from directional ones, and one can understand…”
293 | Fig. 6.15(d): For path b, the uppermost arrowhead should be reversed.
Example 6.8, second paragraph, first line, should read “The cooling rate of the coffee is \( \rho_m V_c \frac{dT}{dt} \). Assuming....”

Example 7.7, first paragraph, next to last line, replace “…heat capacity \( c_p \)” with “…specific heat \( c_p \)”.

In Fig. 7.30, replace \( j = N \) with \( j = J \).

Replace all text beginning after first paragraph in “Black surface enclosures” and ending above Section 7.9.6 with:

Now, \( N \) sample bundle reverse paths are originated from \( dA_k \), and their point of intersection with the enclosure surface at location \( r_j \) is found. Each individual bundle \( n_{j-k} \) is then assigned energy \( w_j = \frac{\left[ \sigma T_j^4(r_j) \right]}{N} \). The value of irradiation on the element \( dA_k \) is then

\[
G(r_k) = \sum_{j=1}^{j} n_{j-k} w_j = \frac{\sigma}{N} \sum_{j=1}^{j} n_{j-k} T_j^4(r_j)
\]

(7.63)

and the local flux \( q_k(r_k) \) is easily found from Equation 7.62.

**Diffuse surface enclosures:** Now, consider an enclosure with nongray but diffuse surfaces. The spectral radiative flux at any wavelength is found from

\[
q_{k,\lambda}(r_k) = J_{k,\lambda}(r_k) - G_{k,\lambda}(r_k)
\]

\[
= \left[ \varepsilon_{k,\lambda} E_{k,\lambda}(r_k) + \left( 1 - \varepsilon_{k,\lambda} \right) G_{k,\lambda}(r_k) \right] - G_{k,\lambda}(r_k) = \varepsilon_{k,\lambda} \left[ E_{k,\lambda}(r_k) - G_{k,\lambda}(r_k) \right]
\]

(7.64)

and the total flux is

\[
q_k(r_k) = \int_{\lambda=0}^{\infty} \varepsilon_{k,\lambda} \left[ E_{k,\lambda}(r_k) - G_{k,\lambda}(r_k) \right] d\lambda - \int_{\lambda=0}^{\infty} \varepsilon_{k,\lambda} G_{k,\lambda}(r_k) d\lambda
\]

(7.65)

Finding the total absorbed radiative flux on nongray–diffuse surface \( dA_k \) then reduces to finding the value of the final integral in Equation 7.65. In reverse Monte Carlo, this is done by again determining the weighted energy of the absorbed incident bundles, assigned by following the reverse bundle paths. Now, however, the energy carried by the bundle is complicated by the interreflections among the diffuse surfaces along the bundle reverse history (Figure 7.31); that is, the radiosity of each surface \( j \) must be taken into account.

The reverse path is followed by initiating the reverse path for \( N \) absorbed bundles on surface \( k \) as for the black case, except that a wavelength must also be assigned to the bundle through Equation 7.52, or for the nongray–diffuse surface \( k \):

\[
R_k = \frac{\int_{\lambda=0}^{\lambda} \varepsilon_{k,\lambda} E_{k,\lambda}(r_k) d\lambda}{\varepsilon_{k,\lambda} T_k^4(r_k)}
\]

(7.66)

Equation 7.66 can be curve fit as for Equation 7.53. Upon intersection of the bundle with an enclosure surface \( j \), a decision is made as to whether the bundle originated at that surface by emission or was reflected from that surface. This is done by next determining the spectral absorptivity of the intersected surface at the wavelength determined from Equation 7.66, \( \alpha_{j,\lambda} = \varepsilon_{j,\lambda} \). A new random number \( R \) is chosen, and if \( R \leq \alpha_{j,\lambda} \), the bundle is assumed to have been emitted by the intersected surface and is assigned the energy \( w_{j,\lambda} = \varepsilon_{j,\lambda} E_{j,\lambda}(r_j) / N \), and its reverse history
is terminated. If, however, \( R > a_{ij} \), the bundle is assumed to have been reflected from the intersected surface, and its history is continued by choosing a further inverse reflected path by choosing the diffuse angles \((\theta_i, \phi_i)\) using the diffuse relations of Equation 7.58 and 7.59. This process is continued through multiple reflections until the location of origin surface \( j \) is found. Many reverse bundle paths \( N \) are then followed from surface \( k \), and the number of these samples diagnosed as leaving surface \( j \) and incident on \( k \), \( n_{j-k} \), is tallied along with their energy, \( w_{j-k} \). Note that detailed balancing requires \( n_{j-k} E_{j} = n_{k-j} E_{j} \).

The integral term in Equation 7.65 is then given by

\[
\int_{\lambda=0}^{\infty} \alpha_{k,j} G_{k,j} \left( r_i \right) d\lambda = \sum_{j=1}^{J} n_{j-k} \int_{\lambda=0}^{\infty} w_{j-k} d\lambda = \sum_{j=1}^{J} \frac{n_{j-k}}{N} \int_{\lambda=0}^{\infty} E_{j,k} E_{j,k} \left( r_j \right) d\lambda
\]

(7.67)

which can be tallied “on the fly” without intermediate storage of \( w_j \) for each bundle.

If the enclosure surfaces are not diffuse, then the reciprocity relations shown for reflectivity can be invoked to allow following reverse paths that account for directional surface properties.

If all surfaces are both gray and diffuse, then substituting Equation 7.67 into Equation 7.65 gives

\[
q_k \left( r_i \right) = e_k \sigma T^4_k \left( r_i \right) - \frac{1}{N} \sum_{j=1}^{J} \alpha_{k,j} n_{k-j} \sigma T^4_k \left( r_j \right) \rightarrow e_k \sigma \sum_{j=1}^{J} \left[ T^4_k \left( r_i \right) - \frac{n_{k-j}}{N} T^4_j \left( r_j \right) \right]
\]

(7.68)

Observe that the forward Monte Carlo approach uses equal-energy bundles and follows their paths from origin to point of absorption and gives the correct angular distribution of irradiation onto the absorbing surface. In contrast, the reverse Monte Carlo procedure assumes a uniform distribution of number of bundles \( N \) in the irradiation but determines the correct angular distribution of irradiation through correctly weighting the energy per incident bundle.

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397 In Fig. 7.31, replace \( j = N \) with \( j = J \).

544 In Eq. (11.26), insert a + between the last two integrals.

769 Line above Eq. (15.37). For nonabsorbing medium, should be: \( k_1 = 0 \).

773 Eq. (15.54): the \( a_j \) and \( b_j \) should not be squared.

774 Eq. (15.58): a multiplier of \( 4\pi \) should replace the 1 in the numerator on the RHS.

916 The reference to Chan, S. and Ge, X.S. should be to Chen, S. and Ge, X.S., and should be reordered alphabetically.